

## 11. System Realization

After a filter is designed, one question is raised: How to implement the filter? In system engineering, we often use the so-called system realization to implement it. Consider a filter is designed as an LTI system described by the following equation:

$$\begin{aligned} y^{(n)}(t) + a_{n-1}y^{(n-1)}(t) + \cdots + a_1\dot{y}(t) + a_0y(t) \\ = b_m u^{(m)}(t) + b_{m-1}u^{(m-1)}(t) + \cdots + b_1\dot{u}(t) + b_0u(t) \end{aligned} \quad (1)$$

which of course is stable. By neglecting the initial conditions, we obtain the frequency response as

$$Y(s) = H(s)U(s) = \frac{b_ms^m + \cdots + b_1s + b_0}{s^n + a_{n-1}s^{n-1} + \cdots + a_1s + a_0}U(s) \quad (2)$$

where  $U(s)$  and  $Y(s)$  are the Laplace transforms of input  $u(t)$  and output  $y(t)$ , and the transfer function is

$$H(s) = \frac{b_ms^m + \cdots + b_1s + b_0}{s^n + a_{n-1}s^{n-1} + \cdots + a_1s + a_0} = \frac{b_m(s - z_1)\cdots(s - z_m)}{(s - p_1)\cdots(s - p_m)} \quad (3)$$

where  $z_j, j=1,2,\dots,m$ , are the zeros and  $p_k, k=1,2,\dots,n$ , are the poles located in the left-half complex plane.

Let's consider  $n > m$  first. It is known that there are an infinite number of ways to realize the system (2) and the most fundamental is to choose state variables as below:

$$X_k(s) = \frac{s^{k-1}}{s^n + a_{n-1}s^{n-1} + \cdots + a_1s + a_0}U(s), \quad k=1,2,\dots,n \quad (4)$$

or

$$X_1(s) = \frac{1}{s^n + a_{n-1}s^{n-1} + \cdots + a_1s + a_0}U(s) \quad (5)$$

$$X_k(s) = s^{k-1}X_1(s) = s^{k-2}X_2(s) = \cdots = sX_{k-1}(s), \quad k=2,3,\dots,n \quad (6)$$

From (5), we have

$$s^n X_1(s) + a_{n-1}s^{n-1}X_1(s) + \cdots + a_1sX_1(s) + a_0X_1(s) = U(s) \quad (7)$$

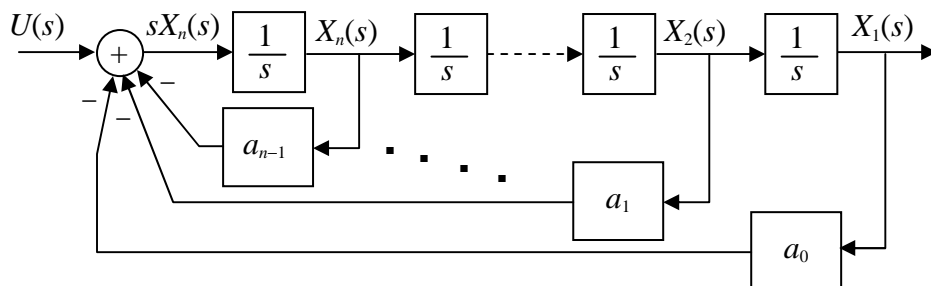
and further from (6) we obtain

$$sX_n(s) + a_{n-1}X_n(s) + \cdots + a_1X_2(s) + a_0X_1(s) = U(s) \quad (8)$$

i.e.,

$$sX_n(s) = -a_0X_1(s) - a_1X_2(s) - \dots - a_{n-1}X_n(s) + U(s) \quad (9)$$

The block diagram is shown as below;



Let  $x_k(t) = \mathcal{L}^{-1}\{X_k(s)\}$ , then from (6) and (9) we have

$$\dot{x}_{k-1}(t) = x_k(t), \quad k=2,3,\dots,n \quad (10)$$

$$\dot{x}_n(t) = -a_0x_1(t) - a_1x_2(t) - \dots - a_{n-1}x_n(t) + u(t) \quad (11)$$

both leading to the following state equation

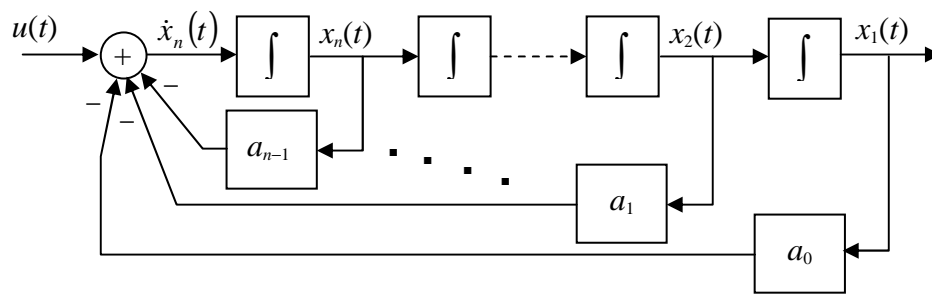
$$\begin{cases} \dot{x}_1(t) = x_2(t) \\ \dot{x}_2(t) = x_3(t) \\ \vdots \\ \dot{x}_{n-1}(t) = x_n(t) \\ \dot{x}_n(t) = -a_0x_1(t) - a_1x_2(t) - \dots - a_{n-1}x_n(t) + u(t) \end{cases} \quad (12)$$

or in the matrix form as

$$\underbrace{\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \\ \dot{x}_3(t) \\ \vdots \\ \dot{x}_{n-1}(t) \\ \dot{x}_n(t) \end{bmatrix}}_{\dot{\mathbf{x}}(t)} = \underbrace{\begin{bmatrix} 0 & 1 & 0 & \dots & 0 & 0 \\ 0 & 0 & 1 & \dots & 0 & 0 \\ 0 & 0 & 0 & \dots & 0 & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & 0 & \dots & 0 & 1 \\ -a_0 & -a_1 & -a_2 & \dots & -a_{n-2} & -a_{n-1} \end{bmatrix}}_{\mathbf{A}} \cdot \underbrace{\begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \\ \vdots \\ x_{n-1}(t) \\ x_n(t) \end{bmatrix}}_{\mathbf{x}(t)} \quad (13)$$

where  $\mathbf{x}(t) = [x_1(t) \ x_2(t) \ \dots \ x_{n-1}(t) \ x_n(t)]^T$  is called the state vector. Similarly,

the corresponding block diagram is shown as below:



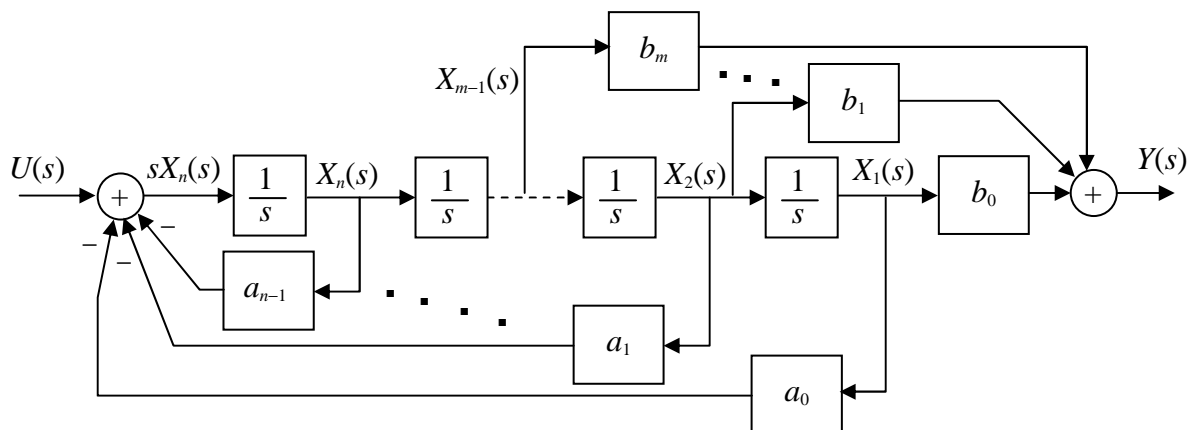
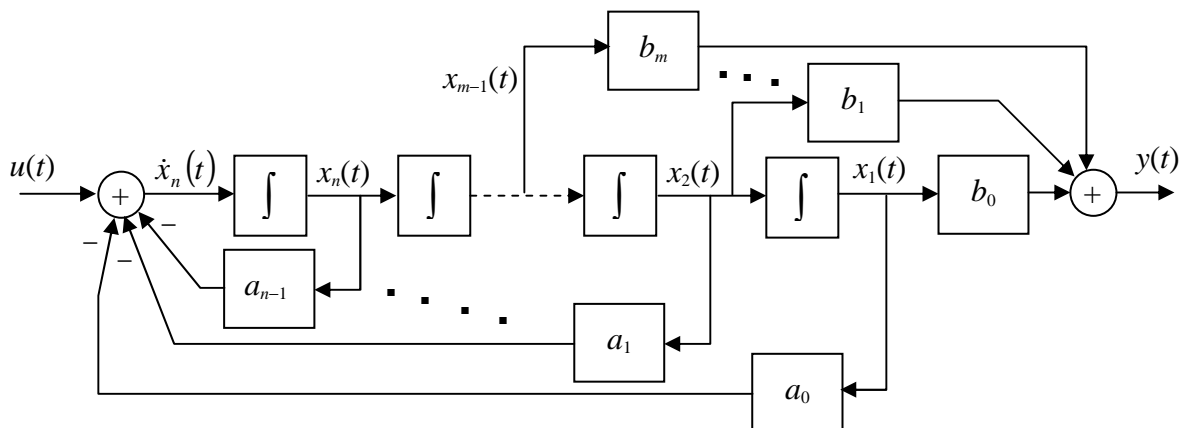
From (2) and (4), the output equation can be derived as

$$Y(s) = b_m X_{m-1}(s) + \dots + b_2 X_3(s) + b_1 X_2(s) + b_0 X_1(s) \quad (14)$$

i.e.,

$$y(t) = b_m x_{m-1}(t) + \dots + b_2 x_3(t) + b_1 x_2(t) + b_0 x_1(t) \quad (15)$$

As a result, the total system can be implemented in time domain or in frequency domain as below:



In the case of  $n=m$ , such as highpass filter, the transfer function is given as

$$H(s) = \frac{b_n s^n + \dots + b_1 s + b_0}{s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0} \quad (16)$$

Rearranging it yields

$$H(s) = b_n + \frac{\beta_{n-1} s^{n-1} + \dots + \beta_1 s + \beta_0}{s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0} \quad (17)$$

where

$$\beta_k = b_k - b_n a_k, \quad k=0,1,2,\dots,n-1 \quad (18)$$

Therefore,

$$Y(s) = H(s)U(s) = \left( b_n + \frac{\beta_{n-1} s^{n-1} + \dots + \beta_1 s + \beta_0}{s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0} \right) U(s) \quad (19)$$

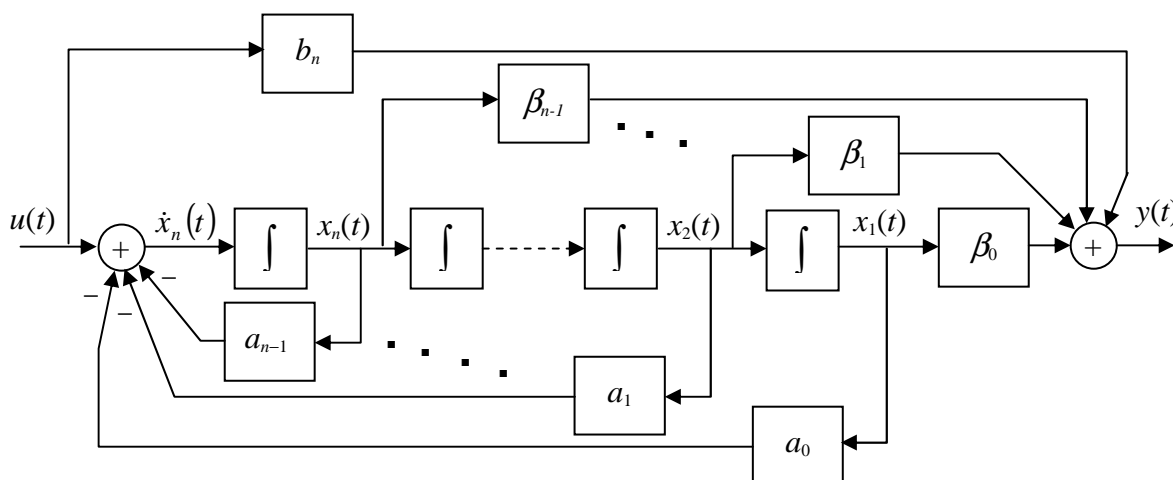
i.e.,

$$Y(s) = b_n U(s) + \beta_{n-1} X_n(s) + \dots + \beta_2 X_3(s) + \beta_1 X_2(s) + \beta_0 X_1(s) \quad (20)$$

or

$$y(t) = b_n u(t) + \beta_{n-1} x_n(t) + \dots + \beta_2 x_3(t) + \beta_1 x_2(t) + \beta_0 x_1(t) \quad (21)$$

The block diagram is



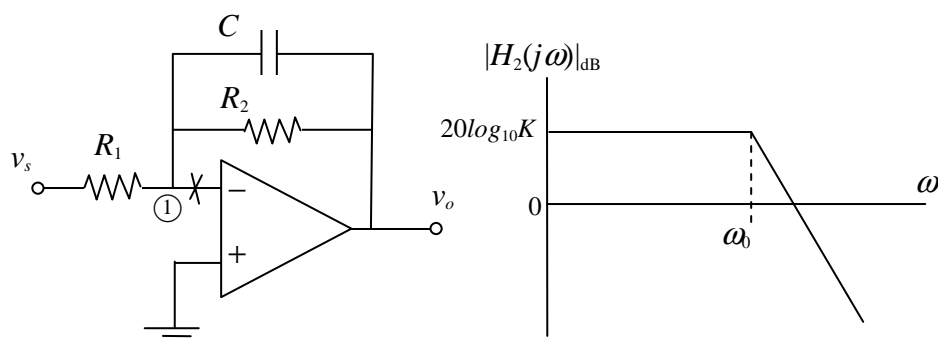
In addition to the above realization, the system can be changed into series, parallel, or a lot of different forms. Most importantly, all of them can be realized by the use of OpAmps.

## [補充教材] 主動式濾波器

一般由  $RLC$  等被動元件所組合而成的濾波器，稱為被動式濾波器，其特性會隨著外接的負載改變，常造成使用上的困擾，為了改進此缺點，具有高輸入電阻與低輸出電阻特性的 OP-amp 便成了最佳的選擇，因為它能夠不受負載變化的影響，此外 OP-amp 為主動式元件，所以將 OP-amp 所設計的濾波器，稱為主動式濾波器。

## ■ 一階低通濾波器

最簡單的主動式一階低通濾波器如圖所示，若單純從電容的阻抗來看，可知在高頻時電容  $C$  可視為短路，使得輸出端的電壓  $v_o(t)$  與節點①的電壓相同，由於節點①為虛擬接地，所以  $v_o(t)=0$ ，即高頻的輸入訊號會被濾除；而在低頻時電容  $C$  可視為開路，此時整個電路形同反相放大器，使得輸出訊號與輸入訊號反相，但大小成正比，即輸入訊號可以順利通過且放大，根據以上的觀察與分析，可以知道它確實是一個低通濾波器。



推導此低通濾波器之轉移函數如下：

$$\frac{V_s(s)}{R_1} = \frac{-V_o(s)}{R_2} + \frac{-V_o(s)}{1/sC} \quad (1)$$

進一步整理後可得

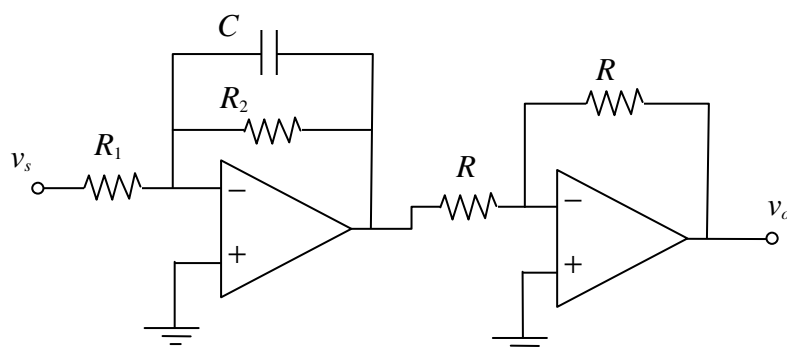
$$H(s) = \frac{V_o(s)}{V_s(s)} = -\frac{R_2}{R_1} \left( \frac{1}{1 + sR_2C} \right) = -\frac{K}{1 + \frac{s}{\omega_0}} \quad (2)$$

其中增益常數  $K = \frac{R_2}{R_1}$ ，截止頻率  $\omega_0 = \frac{1}{R_2C}$ ，其頻率響應  $|H(j\omega)|$  如上圖所示，屬

於低通濾波器，低頻的放大倍率為  $K = \frac{R_2}{R_1}$ ，通常取  $K > 1$ ，即  $R_2 > R_1$ ，故

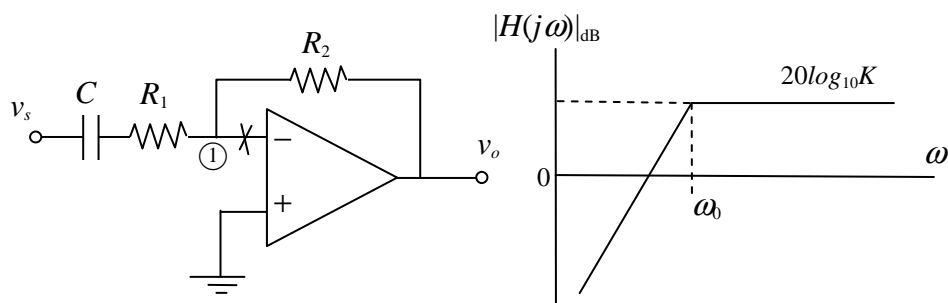
$$|H(j0)|_{dB} = 20 \log_{10} K > 0。$$

若是想要設計輸出訊號與輸入訊號同相的低通濾波器時，只需要再接上一個單位增益的反相放大器即可，如下圖所示。



### ■ 一階高通濾波器

最簡單的主動式一階高通濾波器如下圖所示：



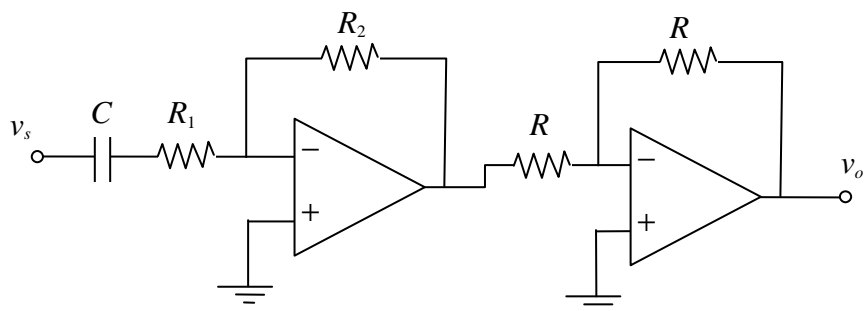
它是在電阻  $R_1$  上串聯一個電容  $C$ ，同樣地可得此電路之轉移函數如下：

$$H(s) = \frac{V_o(s)}{V_s(s)} = -\frac{R_2}{R_1 + \frac{1}{sC}} = -\frac{K(s/\omega_0)}{1 + \frac{s}{\omega_0}} \quad (3)$$

其中增益常數  $K = \frac{R_2}{R_1}$ ，截止頻率  $\omega_0 = \frac{1}{R_1 C}$ ，其頻率響應  $|H(j\omega)|$  如上圖所示，屬

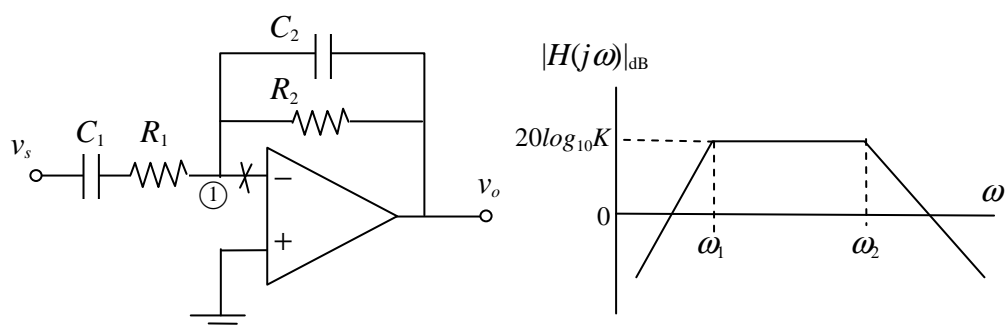
於高通濾波器，放大倍率為  $K$ ，通常取  $K > 1$ ，即  $R_2 > R_1$ ，故  $|H(j\infty)|_{dB} = 20 \log_{10} K > 0。$

若是想要設計輸出訊號與輸入訊號同相的高通濾波器時，仍然只需要再接上一個單位增益的反相放大器即可，如下圖所示：



■ 二階帶通濾波器

主動式二階帶通濾波器如下圖所示：



它在反相放大器的電阻  $R_1$  上串聯一個電容  $C_1$ ，同時在電阻  $R_2$  上並聯一個電容  $C_2$ 。其轉移函數為

$$H(s) = \frac{V_o(s)}{V_s(s)} = -\frac{1}{\left(R_1 + \frac{1}{sC_1}\right)\left(\frac{1}{R_2} + sC_2\right)} \tag{4}$$

$$= -\frac{K(s/\omega_1)}{(1+s/\omega_1)(1+s/\omega_2)}$$

其中增益常數  $K = \frac{R_2}{R_1}$ ，截止頻率  $\omega_1 = \frac{1}{R_1C_1}$  與  $\omega_2 = \frac{1}{R_2C_2}$ ，取  $\omega_2 > \omega_1$ ，則(4)可

改寫為

$$H(s) = -\left(\frac{K(s/\omega_1)}{1+s/\omega_1}\right)\left(\frac{1}{1+s/\omega_2}\right) \tag{5}$$

此式表示  $H(s)$  是由兩個一階濾波器串接而成，其中  $\frac{K(s/\omega_1)}{1+s/\omega_1}$  為高通濾波器，

$\frac{1}{1+s/\omega_2}$  為低通濾波器，其頻率響應如上圖所示。